



FIGS 14.5

14.4 (a) consolidate inner loop first; then obtain overall closed loop transfer function as:

$$y = \psi y_d + \psi_{d_1} d_1 + \psi_{d_2} d_2$$

with

$$\psi = \frac{g_{c_1} \left( \frac{g_{c_2} g_2}{1 + g_{c_2} g_2 h_2} \right) g_1 g}{1 + g_{c_1} \left( \frac{g_{c_2} g_2}{1 + g_{c_2} g_2 h_2} \right) g_1 g h_3 h_1}$$

$$\psi_{d_1} = \frac{g_{d_1}}{1 + g_{c_1} \left( \frac{g_{c_2} g_2}{1 + g_{c_2} g_2 h_2} \right) g_1 h_1 h_3}$$

$$\psi_{d_2} = \frac{\left( \frac{g_{d_2}}{1 + g_2 g_{c_2} h_2} \right)}{1 + g g_1 \left( \frac{g_2 g_{c_2}}{1 + g_2 g_{c_2} h_2} \right) g_{c_1} h_1 h_3}$$

which may be further simplified, if desired.

(b) Consolidate the inner loop first; then obtain overall closed loop transfer function as

$$\psi = \frac{\frac{g g_c}{1 + g_k g_c}}{1 + \frac{g g_c}{1 + g_k g_c}}$$

which simplifies to:

$$\psi = \frac{g^* e^{-\alpha s} g_c}{1 + (g + g_k) g_c} \quad (14.10)$$

so that with  $g_k = g^* - g^* e^{-\alpha s}$ ,  $\psi$  becomes

$$\psi = \frac{g^* g_c e^{-\alpha s}}{1 + g^* g_c}$$

and the characteristic equation,

$$1 + g^* g_c = 0$$

does not include the time delay element.

with  $g_k = 0$ , the characteristic equation is:

$$1 + g^* g_c e^{-\alpha s} = 0$$

which contains the time delay element.

**14.5** If the outputs of each of the parallel processes are designated  $v_1$  and  $v_2$  then

$$y = g_d d + v_1 + v_2$$

$$\text{with } v_1 = g_1 g_{c_1} (y_d - y)$$

$$v_2 = g_2 g_{c_2} (y_d - y)$$

so that

$$y = g_1 g_{c_1} (y_d - y) + g_2 g_{c_2} (y_d - y) + g_d d$$

This rearranges to give

$$y = \psi(s) y_d + \psi_d(s) d \quad (14.11)$$

where

$$\psi = \frac{g_1 g_{c_1} + g_2 g_{c_2}}{1 + g_1 g_{c_1} + g_2 g_{c_2}} \quad (14.12)$$

$$\text{and } \psi_d = \frac{g_d}{1 + g_1 g_{c_1} + g_2 g_{c_2}} \quad (14.13)$$

Now, for there to be no offset, we have the following conditions which  $\psi$  and  $\psi_d$  must satisfy.

$$\lim_{s \rightarrow 0} \psi(s) = 1 \quad (14.14a)$$

$$\text{and } \lim_{s \rightarrow 0} \psi_d(s) = 0 \quad (14.14b)$$

(these conditions may be obtained using the final value theorem of Laplace transforms.)

Under circumstances in which

$g_{c1} = K_{c1}$ , a pure proportional controller

$g_{c2} = \frac{K_{I2}}{s}$ , a pure integral controller

Eq. (14.12) becomes

$$\psi(s) = \frac{sg_1K_{c1} + g_2K_{I2}}{s + sg_1K_{c1} + g_2K_{I2}}$$

$$\text{so that } \lim_{s \rightarrow 0} \psi(s) = \frac{g_2K_{I2}}{g_2K_{I2}} = 1$$

Similarly, Eq. (14.13) becomes

$$\psi_d(s) = \frac{sg_d}{s + sg_1K_{c1} + g_2K_{I2}}$$

$$\text{so that } \lim_{s \rightarrow 0} \psi_d(s) = 0$$

thus establishing that, as required, there will be no offsets.